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Removal of Dust Suppressor and TRU Elements from Wastewaters of Chernobyl NPP Using Synthetic and Natural Flocculants

Abstract #12374

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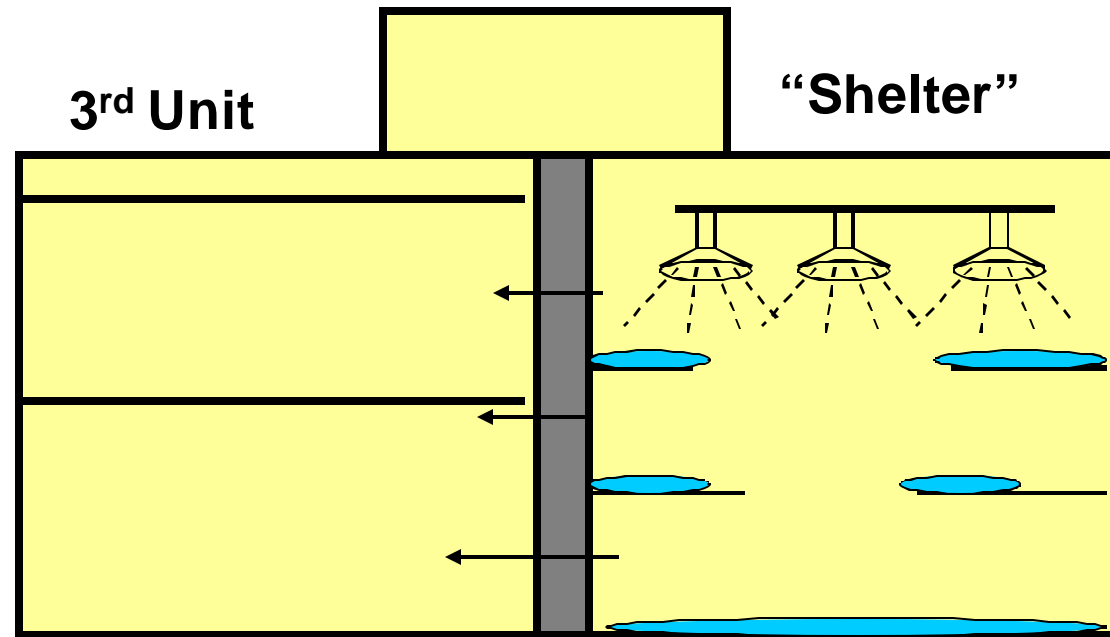
Session #64A

“Task 13 Conceptual Design of the Pre-Treatment Facility for Shelter Water. Report No. TN/01301. Issued 4th May 2000”

IAEA expert missions at ChNPP during 2009-2012 to develop principal technology and pilot test unit to remove organic contaminants and TRU from “Shelter” Object wastewaters

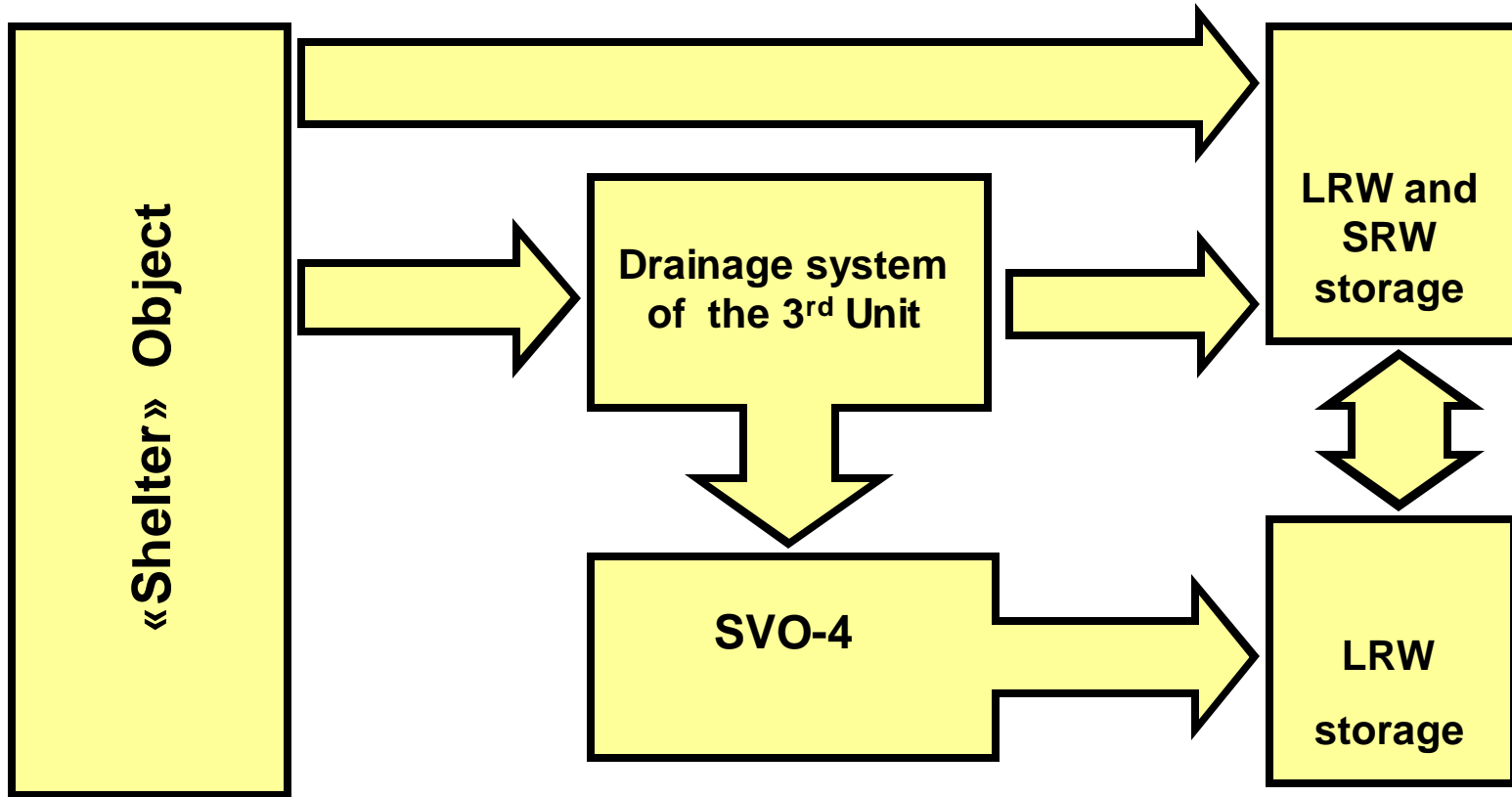
№№ UKR/3/003 12 01, UKR/3/003 12 02, UKR/3/003 12 03,
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Dust Suppressor Emulsion Application at ChNPP



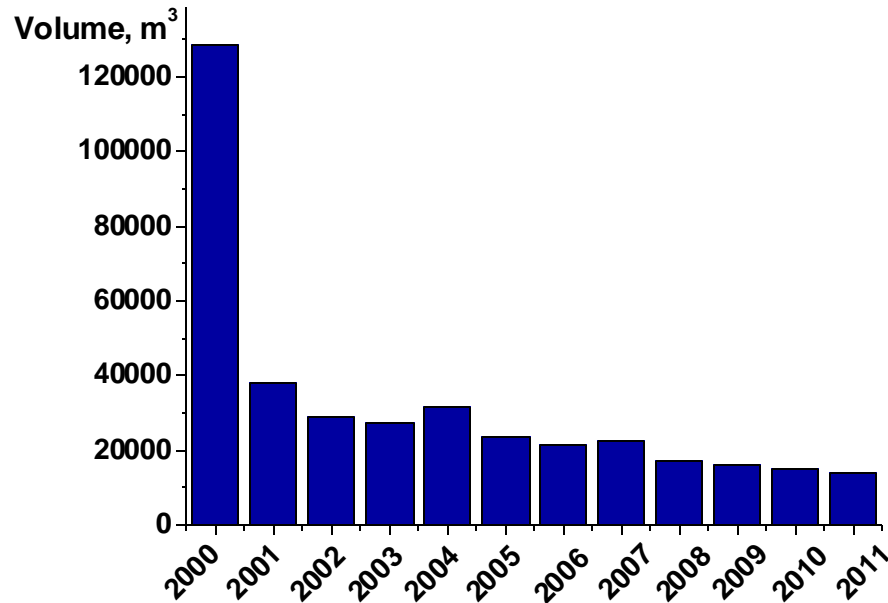
- Sprayed dust suppressor solution and waters after washing spraying system are not separated.
- Non-dried dust suppressor emulsion penetrates down the "Shelter" (Unit 4) rooms to bottom levels and into the adjacent Unit 3 through concrete wall.

ChNPP 3rd and 4th Unit LRW Accumulation Flow Sheet



Dust suppressor containing LRW

3rd and 4th Unit drainage waters



Salinity: <1 g/L

Total α -activity: 1-2 E+04 Bq/kg

Total β -activity: 0.9-4.0E+06 Bq/kg

Dust suppressor content: 0.1-2 g/L



Evaporator concentrates of 3rd and 4th Units drainage waters

Volume at LRW storage:

13 500 m³

Salinity: 300-500 g/L

Total α -activity: 3-4 E+03 Bq/kg

Total β -activity: 3-4 E+07 Bq/kg

Dust suppressor content: ~0.3-0.5 g/L

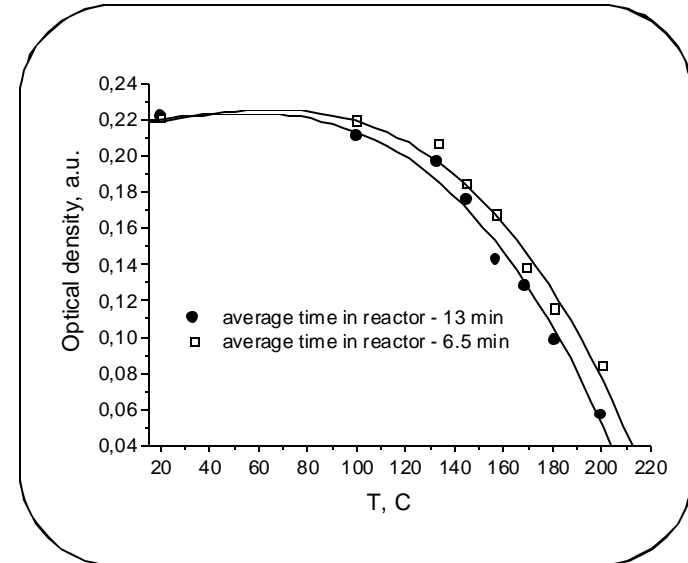
Construction of LRW Treatment Plant is currently suspended

- Designing is 99% completed
- Construction is 98% completed
- Mounting is 97% completed

Problems identified

- Accumulated wastes contain high amounts of dust suppressor and **CANNOT** be treated by evaporation-cementation set up in a new facility.
- TRU content in LRW must be reduced prior to cementation.

Polymerization of dust suppressor under elevated temperature results in formation of virtually insoluble rubber-like deposits on heat-exchangers of the secondary evaporator of SVO-4



**Rubber-like precipitates are formed at
 $T > 130^{\circ}\text{C}$ (salinity > 150 g/L)**

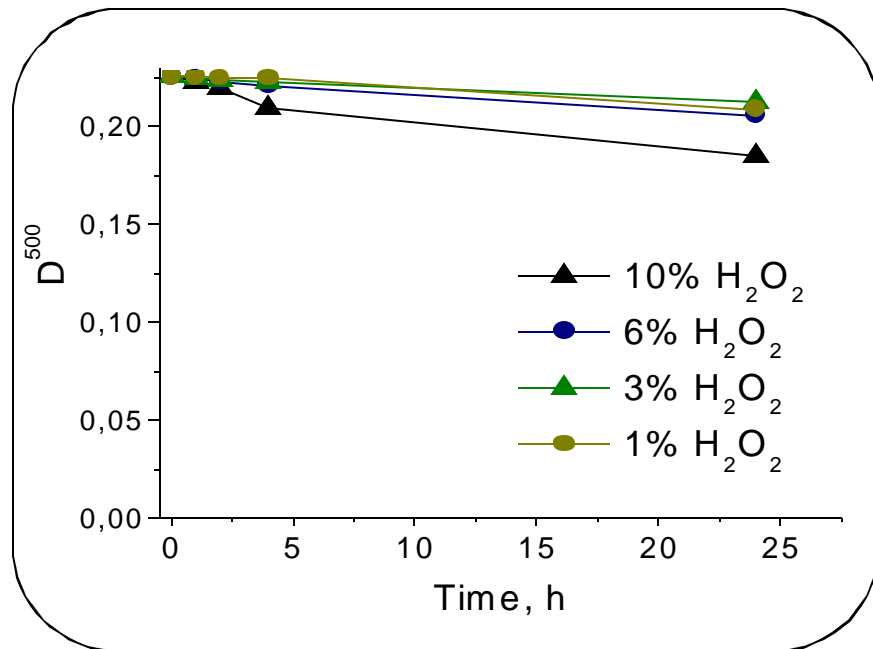
Formation of rubber like precipitates in sealed system of a new LRW Treatment Plant will damage heat exchangers and block facility operation

Possible approaches to remove dust suppressor from LRW

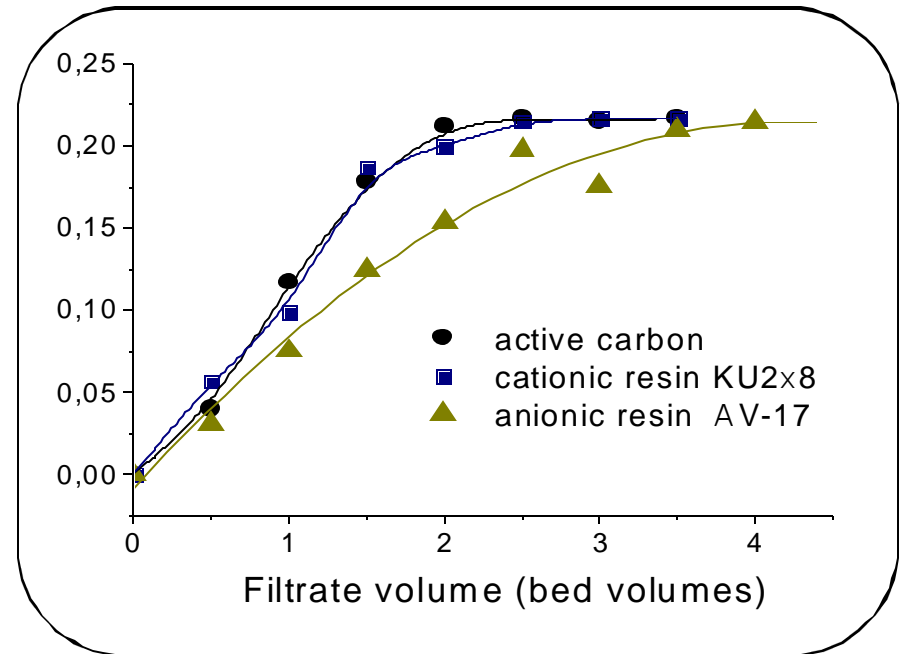
- **Oxidation (ozone, peroxides)**
- **Sorption (active carbon)**
- **Filtration through ion-exchangers**
- **Flocculation with cationic polyelectrolytes**

Removal of Dust-Suppressor

by peroxide oxidation



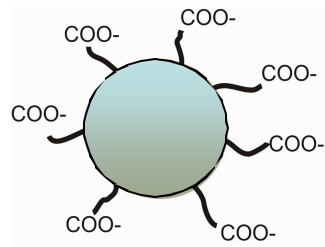
by sorption and ion-exchange filtration



Only up to 10% of dust suppressor can be removed

Required DF > 200

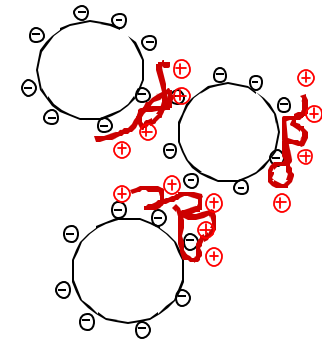
Flocculation/sedimentation setup for dust suppressor and TRU removal



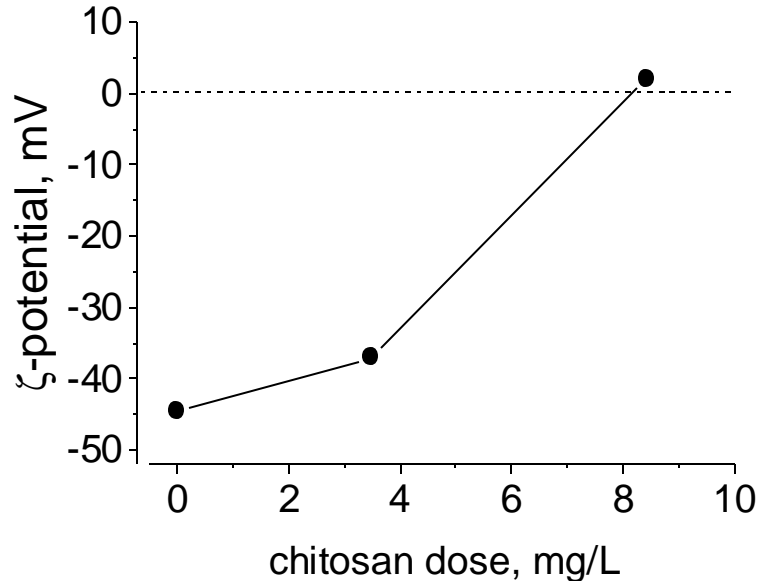
Cationic polymer



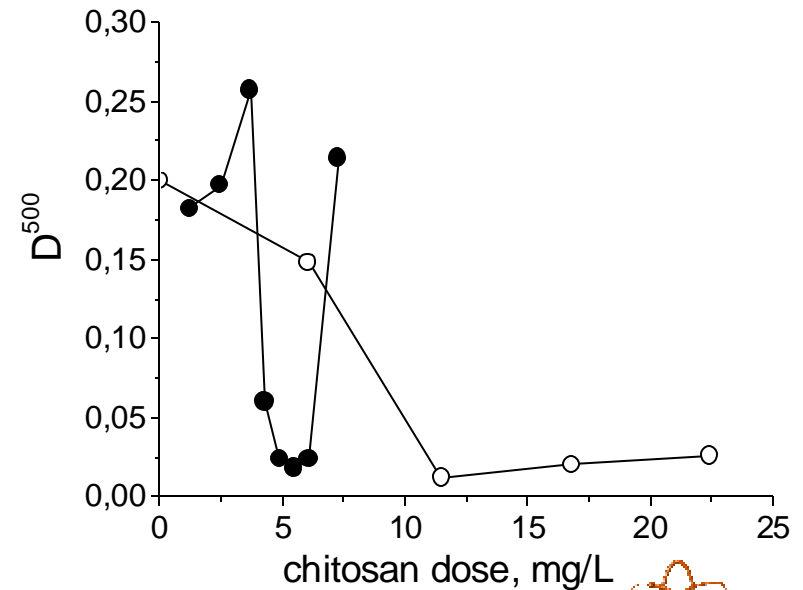
at pH>8 DS coprecipitation
with TRU colloids



Charge neutralization of TRU colloids, pH>8



Dust suppressor removal



Composition of LRW used in the Pilot tests

	<u>pH</u> Dry residue, g/L	<u>[C₂O₄]</u> Oxygen consumption, mg/L	Total <u>α-activity</u> <u>β-activity</u> , Bq/kg	Specific activity, Bq/kg	<u>D⁵⁰⁰</u> DS, mg/L
BTV	<u>9.45</u> 1.10	<u>13.50</u> 220	<u>1.66E+04</u> 9.49E+05	⁶⁰ Co: 3,53E+04 ¹³⁴ Cs: 7,77E+02 ¹³⁷ Cs: 7,54E+05 ¹⁵⁴ Eu: 2,51E+03 ¹⁵⁵ Eu: 1,82E+02 ²⁴¹ Am: 1,30E+04	<u>1.825</u> 233
0005	<u>9.71</u> 0.8	<u>22.5</u> 600	<u>1.30E+04</u> 3.62E+06	⁶⁰ Co: 8,92E+02 ¹³⁴ Cs: 6,94E+02 ¹³⁷ Cs: 2,37E+06 ¹⁵⁴ Eu: 1,80E+03 ²⁴¹ Am: 1,02E+04	<u>2.500</u> 327
201/3 (evaporator concentrate)	<u>11.42</u> 275.4	<u>8730</u> 5000	<u>4.41E+03</u> 3.18E+07	⁶⁰ Co: 8,22E+03 ¹³⁴ Cs: 3,77E+04 ¹³⁷ Cs: 2,63E+07 ²⁴¹ Am: 3,46E+03	0.566 (<u>D¹⁰⁰⁰</u>) 150

Pilot Unit at Chernobyl NPP

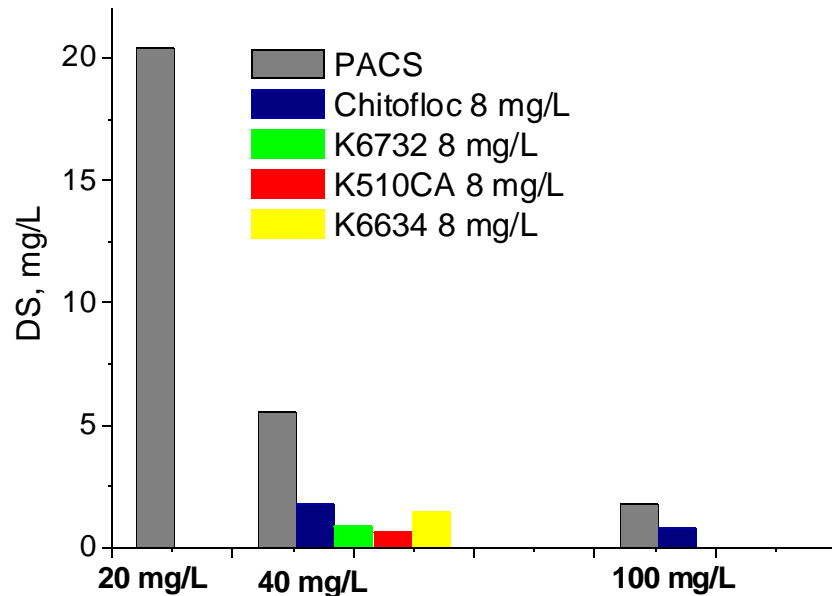


General view of the pilot unit:

service tank (1), precipitation tank (2), accumulation tank (3), membrane pumps for reagents feeding (4), reagent vessels (5), mechanical filters (6), heat-exchanger (7), circulating pumps (8).

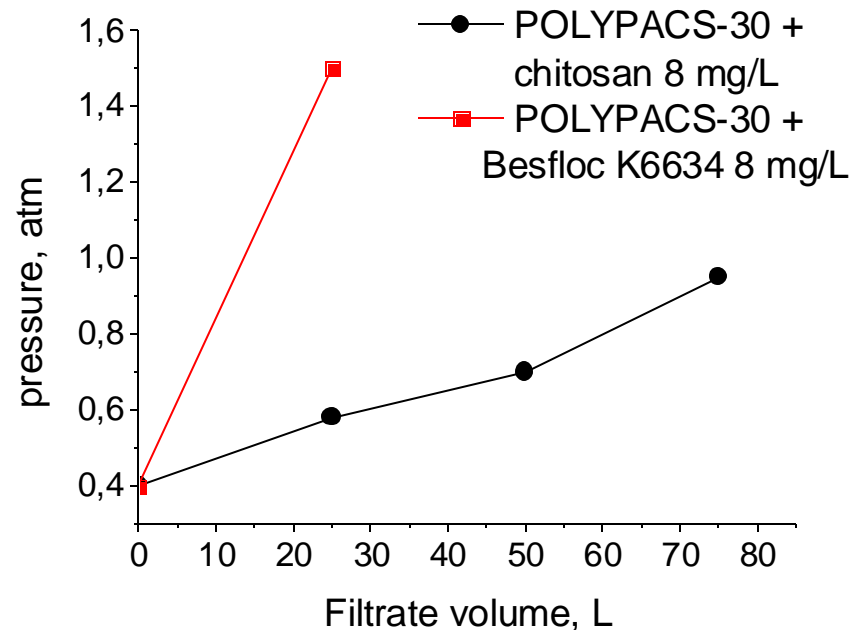
Coagulant/flocculant dose optimization: drainage waters

Residual DS concentration in drainage waters of “Shelter” unit after flocculation



Comparison of chitosan and synthetic flocculants BesFloc (Republic of Korea)

Mechanical filtration of treated LRW



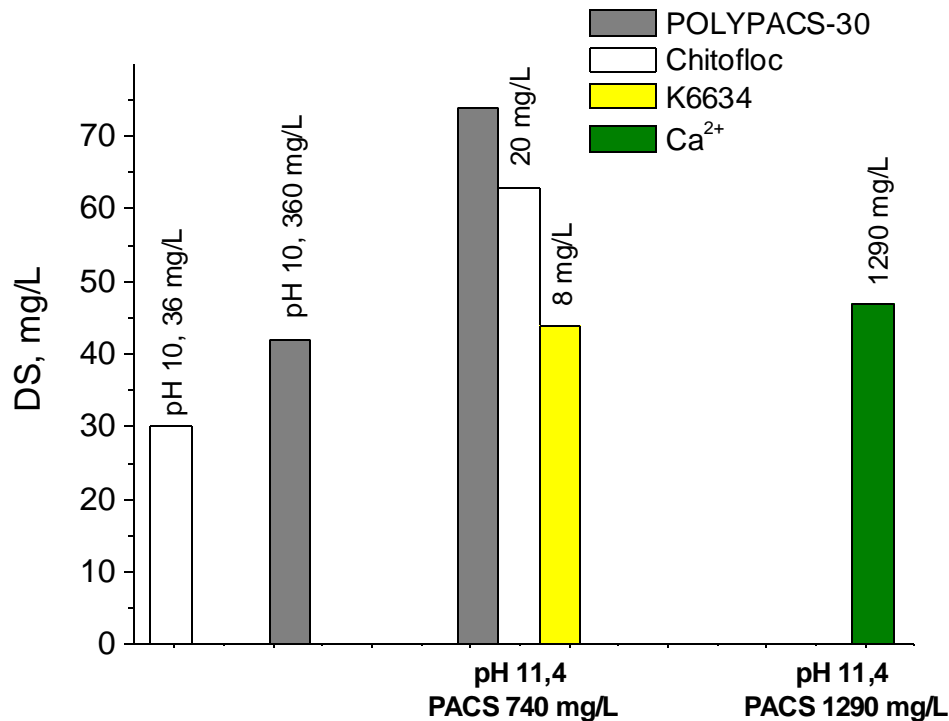
Synthetic flocculants form gel-like precipitates and are not applicable in flocculation-filtration set-up

Sedimentation/Filtration Stage

- **Sedimentation time (flocs ripening) – 5-10 min: continuous process is possible**
- **Mechanical filtration rate is 10 to 120 L/h (filters – 2 dm³ each)**

**Filtration media tested:
sand, ion-exchangers «Dowex Monosphere» - cation-exchanger (650NG) and anion-exchanger (550NG) mixed at ratio 1:1.5 to simulate spent ion-exchange resins available at ChNPP**

Coagulant/flocculant dose optimization: evaporator concentrates



Reagents tested

- PACS
- chitosan
- BesFloc cationic flocculants
- addition of calcium salts to suppress oxalate effect

Decontamination factor for DS is 5-10

Due to the lack of electrostatic interactions in high salinity media (>200 g/L) flocculation/sedimentation set-up is not efficient for evaporator concentrates

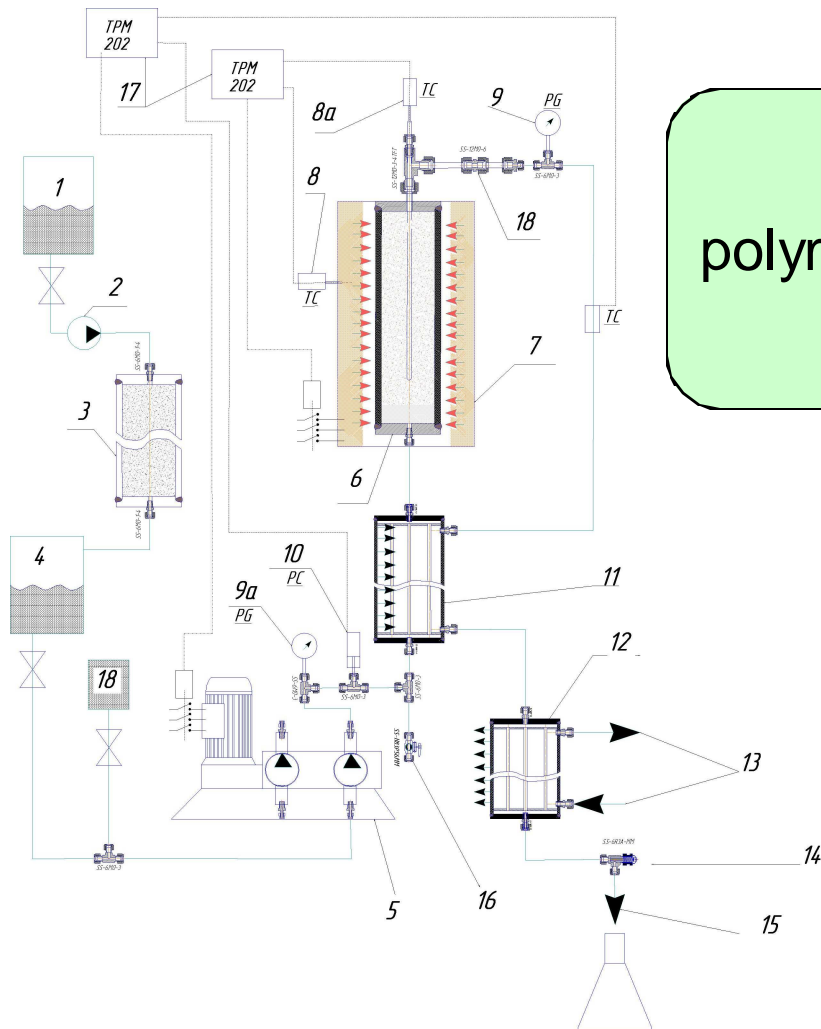
Selected Pilot Test Results

Sample	Reagent dose	D ⁵⁰⁰ (filtrate) ————— DS content, mg/L	Total β-activity, Bq/kg	Total α-activity Bq/kg
Experiment №1 BTV	POLYPACS 200 mg/L Chitofloc 7.8 mg/L	0.053 ————— 5.51	6.11E+5	n/detected
Experiment №2 BTV	POLYPACS 125 mg/L	0.015 ————— 0.64	7.05E+5	n/detected
Experiment №3 0005	POLYPACS 260 mg/L Chitofloc 10 mg/L	0.029 ————— 2.43	1.77 e+6	n/detected

**Decontamination factors for drainage waters:
DS>500, TUE>1000**

How to treat 13 500 m³ of dust suppressor containing evaporator concentrate?

Possible solution:
polymerization of DS under hydrothermal conditions before evaporation



Main subunits of the hydrothermal unit

- 1 – feeding tank
- 2, 5 – pumps
- 3 – sorption filter for cesium removal
- 4 – tank for treated wastes collection
- 6 – hydrothermal reactor
- 7 – oven
- 8 – thermocouple
- 12 – cooler

Hydrothermal Unit of the Pilot Unit at ChNPP



Treatment conditions

$T = 270-310^{\circ}\text{C}$

$P = 80-100 \text{ bar}$



evaporator concentrate
before treatment

PROSPECTS

